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## 教育事務委員會 <br> 2021年1月8日會議跟進事宜

## 8021EM一於青衣興建職業訓練局航空及航海教育中心

你於2021年1月8日就當日教育事務委員會會議的跟進事宜致教育局局的來函收悉。有關職業訓練局（職訓局）擬於青衣發展航空及航海教育中心（教育中心）的補充資料現載列如下，供委員参閱。

## 職䚯局的航空及航海相關課程的補充資料

2．目前，職訓局開辦一共 20 個與航空及航海相關的課程。由於缺乏相應的專門訓練設施，現時有關課程的實務訓練分散於職訓局不同的校舍内舉行，包括香港專業教育學院，青年學院及海事訓練學院的校舍。因應航空及航海業界的人力需求，以及現時

供學生使用的實務訓練設施不足，職訓局建議興建教育中心，為學生提供優質及模擬真實工作環境的訓練體驗，支持本港航空及航海業長遠的人力需求。擬建的教育中心將設置嶄新的培訓設施，如航空工程和航空器系統維修培訓工場，以及海事工程實驗室，以期裝備畢業生考取民航處頒發的航空器維修基本執照，或海事處發出的本地船舶輪機操作員合格證明書，投身相關行業。

3．在擬建的教育中心投入運作後，有關課程的學員將可集中於位於香港專業教育學院青衣分校的教育中心進行有關的實務訓練，善用其嶄新培訓設施 。長遠而言，職訓局亦計劃因應業界的人力需求，考慮開辦適切的新課程 ${ }^{1}$ 。然而，職訓局會通過課程及課堂編配等安排，確保於香港專業教育學院青衣分校的規劃入學人數維持於 2020 年的水平，即約 7500 人。有關與航空及航海相關課程的資料載於附件一。

## 航空及航海業的人力需求及課程畢業生前景

4．就航空業的未來人力需求方面，香港機場管理局預計在 2030 年三跑道系統啟用後，於機場區域所提供的直接職位將增至 141000 個，較現時增加超過一倍。此外，職訓局在進行行業人力調查後作出的 2020 年人力更新報告亦指出，飛機維修工程行業於對技術員及技師人手需求甚殷，而其機電工程業的人力更新報告亦指出，2018年下半年至2019年上半年期間的飛機維修工程相關空缺超過 100 個，反映飛機維修行業對員工增補有相當需求。

5．雖然航空業受到意料之外的疫情影響，而疫情所带來的負面影響預計仍將持續一段時間，但職訓局預期待疫情受控後，航空業將會逐步回復正常。根據國際航空運輸協會於2020年7月發表的報告中，航空業的客運量預計將於2024年稍後時間回復至 2019 年的相若水平，而事實上2020年的貨物空運量亦僅比 2019年同期略為下跌約 $10 \%$ ，有望更早復甦。職訓局亦預計，由於教育中心的建築需時約三年半，在教育中心完工並投入運作後，將配合屈時全球及本港航空業復蘇，回應業界預期對人力及相應培訓的逼切需求。

[^0]6．在航海業的人力需求方面，職訓局在進行行業人力調查後作出的2016年人力調查報告和2020年人力更新報告均顯示，航海業的人手老化問題嚴重，業界對具執照的在岸工作海事工程技術員及工程師有極大需求。隨著現職海事工程技術人員於未來5至10年陸續退休，航海業預計將出現約1000個空缺。事實上，輪機工程師及船舶總管已被列入「優秀人才入境計劃」下的人才清單，可見香港對有關專業人才需求殷切。

7．就航空及航海相關課程的畢業生前景方面，職訓局的數字顯示，有關畢業生的升學及就業情況理想，反映課程及其學員的質素獲行業及其他專上院校普遍認同。具體而言，在航空相關課程畢業生方面，過去五年，55\％畢業生選擇繼續升學，其中 $86 \%$獲香港高等教育科技學院，香港理工大學和香港科技大學等本地院校取錄入讀相關學士學位課程。其稌選擇直接就業的畢業生當中，超過 $95 \%$ 成功入職航空業。至於航海相關課程方面，超過 $95 \%$ 的畢業生選擇直接就業，平均就業率約 $83 \%$ ；其稌選擇繼續升學的畢業生則獲本地及海外大學，如香港理工大學和英國普利茅斯大學，取錄入讀相關海事學士學位課程。

8．為支援畢業生就業，職訓局過去十多年一直舉辦事業啟航計劃，鼓勵學生参觀業内公司，與機構人員進行小組討論，並提供適切的就業輔導服務，讓學生瞭解個人的職業性向和事業目標。在疫情期間，職訓局亦加強有關支援，包括為學生安排線上職業講座，加深學生對未來的職業前景的瞭解。職訓局會繼續有關工作，並會因應疫情及職場的情況作出適當跟進。

## 境外交流，實習及工作機會

9．除了於香港授課外，職訓局亦安排其學生到境外參加各類型的交流，實習等活動，例如舉辦大灣區的交流及参觀活動，通過讓學生接觸區内不同機構，擴闊他們的眼界及就業機會。舉例而言，職訓局會協助及鼓勵學生參加每年與廣州民航職業技術學院合辦的飛機維修工程技能比賽，大連海事大學的培訓課程，参觀廣州飛機維修工程有限公司等，加深學生對香港以外的工作環境的認識。雖然有關境外的活動受疫情影響，但職訓局亦積極計劃更多相關活動，例如職訓局正籌劃安排學生参觀澳門的院校和機構，以更深入瞭解大灣區各城市的相關行業發展。

## 擬建教育中心可能造成的交通影響

10．職訓局於2020年就項目委聘專業交通顧問進行交通影響評估。儘管教育中心將提供崭新的培訓設施，為學生提供以往未能提供的實務䚯練，但職訓局將透過重新安排課程及課堂等安排，確保未來於香港專業教育學院青衣分校校園上課的學生總數會與目前水平相若。故此，有關項目並不會增加前往該校園的學生人數，亦不會為該區带來額外的交通流量，而對公共運輸服務的需求亦會維持於現有水平。交通顧問早前亦評估了教育中心運作後對路口容車量和行人的影響，結果指出鄰近所有的主要路口和行人路於繁忙時段的表現均令人霂意，而整體交通影響評估的結果總結出擬建發展不會對交通，行人網絡和公共運輸服務带來負面影響。詳細交通影響評估載於附件二。

教育局局長
（吴肇基


代行）

2021年2月9日

## 附件一

職剖局現有和計劃開辨的航空及航海相關的課程

| 現有課程 | 課程性質 | 2020／21 <br> 學年規 <br> 劃入學 <br> 人數 | 2020／21 <br> 學年實 <br> 際入學 <br> 人數 | 2025／26 <br> 學年規 <br> 劃入學 <br> 人數 |
| :---: | :---: | :---: | :---: | :---: |
| 航 空 |  |  |  |  |
| 飛機工程（榮譽）工學士 （註1） | 職前資助課程 | 56 | 38 | 60 |
| 飛機維修工程高級文憑 <br> （註1） | 職前資助課程 | 120 | 112 | 125 |
| 飛機維修工程高級文憑 | 在職自資課程 | 56 | 不適用 （註 2） | 60 |
| 職專文憑（飛機維修） <br> （註1） | 職前資助課程 | 50 | 62 | 90 |
| 職專文憑（飛機維修） | 在職自資課程 | 28 | 不適用 （註 2） | 30 |
| 航空學高級文憑（註 1） | 職前資助課程 | 60 | 44 | 90 |
| 航空及電子物流高級文憑 | 職前資助課程 | 30 | 24 | 80 |
| 航空服務及客運管理高級文憑（註1） | 職前資助課程 | 30 | 57 | 100 |
| 基礎課程文憑（航空） | 在職自資課程 | 30 | 4 | 50 |
| 總數 |  | 460 | 341 | 685 |
| 航海 |  |  |  |  |
| 機械工程學高級文憑 （輪機選修科） | 職前資助課程 | 不適用 | 8 | 30 |
| 海事科技高級文憑 <br> （註1） | 職前資助課程 | 60 | 43 | 45 |
| 初級全能海員證書 | 職前資助課程 | 80 | $\begin{gathered} 28 \\ (\text { 註 } 2 \text { ) } \end{gathered}$ | 80 |
| 三級（甲板高級船員） <br> （遠洋）適任證書培訓提 | 在職自資課程 | 22 | $\begin{gathered} 19 \\ (\text { 註 } 2) \end{gathered}$ | 110 |


| 現有課程 | 課程性質 | 2020／21 <br> 學年規 <br> 劃入學 <br> 人數 | 2020／21 <br> 自年實 <br> 際入學 <br> 人數 | 2025／26 <br> 學年規 <br> 劃入學 <br> 人數 |
| :---: | :---: | :---: | :---: | :---: |
| 升課程（註 1） |  |  |  |  |
| 二／一級（甲板高級船員） （遠洋）適任證書培䚯提升課程（註1） | 在職自資課程 | 18 | $\begin{gathered} 6 \\ \left(\begin{array}{c} \text { (註 } 2 \end{array}\right) \end{gathered}$ | 100 |
| 海事業高壓電力科技 （註1） | 在職自資課程 | 5 | 2 | 10 |
| 海事資源管理課程 | 在職自資課程 | 43 | $\begin{gathered} 17 \\ (\text { 註 } 2 \text { ) } \end{gathered}$ | 50 |
| 本地船舶三級輪機操作員（註 1） | 在職自資課程 | 14 | $\begin{aligned} & \text { 不適用 } \\ & \left(\begin{array}{c} \text { 註 } 2) \end{array}\right. \end{aligned}$ | 90 |
| 本地船舶二級輪機操作員（註 1） | 在職自資課程 | 12 | $\begin{aligned} & \text { 不適用 } \\ & \text { (註 2) } \end{aligned}$ | 10 |
| 本地船舶三級船長 （註1） | 在職自資課程 | 58 | $\begin{gathered} 21 \\ (\text { 註 } 2 \text { ) } \end{gathered}$ | 180 |
| 本地船舶二級船長 （註1） | 在職自資課程 | 14 | $\begin{aligned} & \text { 不適用 } \\ & \text { (註 2) } \end{aligned}$ | 15 |
| 總數 |  | 326 | 144 | 720 |

註1：將於航空及航海教育中心進行實務訓練
註 2：2020／21學年稍後時間繼續收生

| 計劃開辦的課程 | 課程性質 | 2025／26 <br> 學年規劃 <br> 入學人數 |
| :---: | :---: | :---: |
| 航 空 |  |  |
| 飛機維修技術及實務證書（註） | 職前資助課程 | 28 |
| 飛機維修技術及實務證書 | 在職自資課程 | 28 |
| 航空智運專業文憑 | 在職自資課程 | 27 |
| 航空管理專業文憑 | 在職自資課程 | 27 |
| 總數 |  | 110 |
| 航海 |  |  |
| 海事及遊艇科技高級文憑（註） | 職前資助課程 | 30 |
| 職專文憑（海事） | 職前資助課程 | 20 |
| 總數 |  | 50 |

註：將於航空及航海教育中心進行實務訓練

# Vocational Training Council Proposed Aviation and Maritime Education Centre 

## Tsing Yi

Traffic Impact Assessment Study
Final Report

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Figure 4-2 Locations of Planned / Committed Developments
Figure 4-3 2028 Design Peak Hour Traffic Flows

## APPENDICES

Appendix A 2020 Junction Calculation Sheets<br>Appendix B 2028 Junction Calculation Sheets

## 1 INTRODUCTION

## $1.1 \quad$ Background

1.1.1 The Vocational Training Council (VTC) intend to redevelop the northern portion of the existing VTC Campus in Tsing Yi ("the VTC TY Campus") for an Aviation and Maritime Education Centre ("the Proposed AMEC") which will provide workshops, laboratories, teaching facilities, staff offices and associated facilities to support the training and manpower development of the aircraft and marine industries.
1.1.2 A Traffic Impact Assessment (TIA) Study had been undertaken in 2017 to assess the potential traffic impact to be induced by the Proposed AMEC and the findings reported in "Technical Study for Aircraft and Marine Engineering Centre at Tsing Yi Campus Traffic Impact Study (November 2017)" concluded that the local road network would be able to cope with the additional AMEC traffic.
1.1.3 Ozzo Technology (HK) Limited have been commissioned to review and update the Traffic Impact Assessment (TIA) Study based on the latest development parameters and taking into account the latest developments in the Study Area.

### 1.2 Study Objectives

1.2.1 The objectives of the TIA study are as follows:

- To review the existing traffic situation of the surrounding road network;
- To estimate the potential traffic generations/attractions to be induced by the Proposed AMEC;
- To assess the future traffic situation of the surrounding road network;
- To appraise the potential traffic impact of the Proposed AMEC on the surrounding road and pedestrian networks and to recommend improvement proposals, if required.

Traffic ImpactAssessment Study

### 1.3 Report Structure

1.3.1 Following this introductory chapter, this report is arranged as follow:

- Chapter 2 describes the Proposed AMEC;
- Chapter 3 summarizes the existing traffic condition in the vicinity of the Proposed AMEC;
- Chapter 4 provides traffic forecast in the future design year and presents the traffic assessment results;
- Chapter 5 discusses the results of the pedestrian impact assessment and public transport review; and
- Chapter 6 summarizes the findings and conclusion of this study.


## 2 THE PROPOSED AMEC

### 2.1 Site Location and Study Area

2.1.1 Figure 2-1 shows the location of the Proposed AMEC within the existing VTC Campus. At present, the VTC TY Campus comprises mainly of Hong Kong Institute of Vocational Education (Tsing Yi), Technological and Higher Education Institute of Hong Kong and Hall of Residence. As shown in the figure, the Proposed AMEC will be situated at the existing tennis courts situated at the northern portion of the VTC TY Campus.
2.1.2 Figure 2-1 also shows the proposed Study Area for this TIA Study and which includes the key junctions in the vicinity of the Project Site.

### 2.2 The Proposed Development Schedule

2.2.1 Similar to the existing facilities in the VTC TY Campus, the proposed AMEC will provide workshops, laboratories, teaching facilities and associated facilities to support the training and manpower development of the aircraft and marine industries.
2.2.2 Table 2-1 summarizes the number of student places and staff in the existing VTC Campus and with the new provisions upon completion of the Proposed AMEC.

Table 2-1 Numbers of Student and Staff Places at Existing and Future VTC Campus

|  | 2020 VTC TY Campus(1) | VTC TY Campus |
| :--- | :---: | :---: |
| with new AMEC |  |  |

2.2.3 In 2020, there are a total of 7,654 student places (5,087 full-time and 2,567 part-time) and 947 staff members ( 629 full-time and 318 part-time) in the existing VTC TY Campus. The new AMEC can provide practical training to 1,000 students in each academic year. The numbers of these 1,000 students have been included in the overall total of 8,601 as indicated above because they come from the related programmes offered at the existing TY Campus.

### 2.3 Access Arrangements

2.3.1 Figure 2-2 shows the vehicular and pedestrian access arrangements at the VTC TY Campus after the completion of the Proposed AMEC. In general, all the existing vehicular and pedestrian accesses at VTC TY Campus will be maintained.

### 2.4 Internal Transport Facilities

2.4.1 As the Proposed AMEC consists mainly of workshops and laboratories, the demand for car parking and loading/ unloading will be very small and can be shared with the existing facilities available in the existing VTC TY Campus. Hence, no parking and loading/unloading facility will be provided within the Proposed AMEC.

## 3 EXISTING TRAFFIC CONDITIONS

### 3.1 Existing Road Network

3.1.1 Figure 2-1 shows the existing road network in the Study Area.
3.1.2 The Proposed AMEC can be accessed via Sai Shan Road which is a local road, in single-2 lane carriageway standards, providing accesses to nearby developments along the road. Sai Shan Road connects with Tsing Yi Road, a District Distributor road in dual-2 lane carriageway standards, which is a major north-south corridor in Tsing Yi Island.
3.1.3 The section of Tsing Yi Road in the vicinity of VTC TY Campus connects with Ching Hong Road, a Local Distributor road, to provide access to/from the west. Tsing Yi Road also links with Tsing Yi Bridge/ Kwai Tsing Road connecting Tsing Yi Island with Kwai Chung district and urban Kowloon.

### 3.2 Existing Public Transport Services

3.2.1 The area is well served by public transport services with both franchised bus and Green Minibus services. Table 3-1 summarized the public transport services in the area and Figure 3-1 shows the locations of the bus/GMB stops serving the area.
3.2.2 In addition, shuttle bus services providing connecting services between VTC TY Campus and MTR Kwai Fong Station and Tai Wai Station are available for VTC students and staff.

Table 3-1 Existing Public Transport Services in the Study Area

| Route No. | Termination Points |  | Frequency (Mins) |
| :---: | :--- | :--- | :--- |
| Franchised Bus Services |  |  |  |
| KMB 41 | Tsing Yi (Cheung Ching Estate) | Kowloon City Ferry | Daily service every 25-35 mins |
| KMB 42 | Tsing Yi (Cheung Hong Estate) | Shun Lee | Daily service every 15-25 mins |
| KMB 42A | Tsing Yi (Cheung Hang Estate) | Jordan (West Kowloon <br> Station) | Daily service every 4-15 mins |
| KMB 43 | Tsing Yi (Cheung Hong Estate) | Tsuen Wan West <br> Station | Daily service every 8-20 mins |
| KMB 43A | Tsing Yi (Cheung Wang Estate) | Shek Lei <br> (Tai Loong Street) | Daily service every 6-15 min |
| KMB 43C | Tsing Yi (Cheung Hong Estate) | Island Harbourview | Daily service every 12-15 mins <br> during AM and PM peak periods |
| KMB 43D | Tsing Yi (Cheung Wang Estate) | Kwai Shing | Two departures daily during AM <br> peak hour |
| KMB 43M | Kwai Fong Station | Cheung Ching Circular) | Daily service every 12-20 mins |


| Route No. | Termination Points |  | Frequency (Mins) |
| :---: | :--- | :--- | :--- |

### 3.3 Existing Peak Hour Traffic Flows

3.3.1 Due to the outbreak of COVID-19 disease in 2020, the traffic conditions in the HKSAR territories are significantly affected as a result of the government preventive and control measures such as school break, suspension of school activities, home office practice, restriction or compulsory quarantine for people entering Hong Kong etc. Hence, reference is made to the traffic count data obtained in $2017^{1}$, which were observed under normal traffic conditions and school activities, for subsequent analysis.

[^1]3.3.2 The traffic count surveys were undertaken at the key links and junctions in the Study Area of the Project Site during the AM and PM peak periods on a typical weekday in September 2017. Figure 3-2 shows the locations of the surveyed key links and junctions. The AM and PM peak hours are identified to occur at 08:30-09:30 and 17:30-18:30 respectively and the 2017 observed peak hour traffic flows on the road network in the vicinity of the Project Site are shown in Figure 3-3.
3.3.3 The 2017 peak hour traffic flows are then adjusted to derive the 2020 traffic flows taking into account the historical traffic data in the vicinity of the Site as indicated in Table 3-2.

Table 3-2 Average Annual Daily Traffic from Annual Traffic Census

| Station | Road | Between |  | 2013 | 2014 | 2015 | 2016 | 2017 | 2018 | Average Growth Rate p.a. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 5653 | Ching Hong Rd | Chung Mei Rd | Tsing Yi Rd | 11,290 | 11,390 | 13,200 | 11,560 | 11,770 | 11,950 | 1.14\% |
|  |  |  |  | -- | 0.89\% | 15.89\% | -12.42\% | 1.82\% | 1.53\% |  |
| 6219 | Kwai Tsing Rd \& Tsing Yi S Bridge | Tsing Yi Rd | Kwai Tai Rd Interchange | 47,000 | 44,770 | 46,950 | 41,880 | 40,920 | 42,080 | -2.19\% |
|  |  |  |  | -- | -4.74\% | 4.87\% | -10.80\% | -2.29\% | 2.83\% |  |
| 5232 | Tsing Yi Rd | Tsing Yi Heung Sze Wui Rd | Ching Hong Rd | 18,980 | 20,560 | 20,950 | 21,530 | 21,920 | 19,550 | 0.59\% |
|  |  |  |  | -- | 8.32\% | 1.90\% | 2.77\% | 1.81\% | -10.81\% |  |
| 5852 | Tsing Yi Heung Sze Wui Rd | Fung Shue Wo Rd Roundabout | Tsing Yi Rd | 31,770 | 32,040 | 32,640 | 33,300 | 32,890 | 33,380 | 0.99\% |
|  |  |  |  | -- | 0.85\% | 1.87\% | 2.02\% | -1.23\% | 1.49\% |  |
| 5439 | Tsing Yi Rd | Ching Hong Rd | Tsing Nam St | 6,890 | 7,080 | 7,170 | 7,370 | 7,500 | 7,620 | 2.03\% |
|  |  |  |  | -- | 2.76\% | 1.27\% | 2.79\% | 1.76\% | 1.60\% |  |
| 6113 | Tsing Yi Rd | Tsing Yi Rd near Dow Chemical | Tsing Yi Hong Wan Rd | 10,920 | 11,020 | 11,220 | 11,540 | 12,870 | 11,720 | 1.42\% |
|  |  |  |  | --\% | 0.92\% | 1.81\% | 2.85\% | 11.53\% | -8.94\% |  |
| 6112 | Tsing Yi Hong Wan Rd | Tsing Yi Rd | Tsing Sheung Rd | 18,770 | 18,930 | 19,280 | 19,820 | 20,750 | 25,970 | 6.71\% |
|  |  |  |  | -- | 0.85\% | 1.85\% | 2.80\% | 4.69\% | 25.16\% |  |
| Total |  |  |  | 145,620 | 145,790 | 151,410 | 147,000 | 148,620 | 152,270 | 0.90\% |
|  |  |  |  | -- | 0.12\% | 3.85\% | -2.91\% | 1.10\% | 2.46\% |  |

Source: 2013-2018 Annual Traffic Census (ATC) Reports published by Transport Department
3.3.4 As indicated in the Table 3-2, an overall traffic growth of $0.9 \%$ per annum was recorded over the period of 2013-2018. However, to provide conservative estimates, it is proposed to apply the higher growth rate of $+2.46 \%$ p.a. (i.e. the growth rate from 2017 to 2018) for deriving the 2020 peak hour Flows. By applying the annual growth rate (+2.46\%) to the 2017 observed peak hour flows, the derived 2020 Peak Hour Traffic Flows are shown in Figure 3-4.
3.3.5 For reference, the peak hour performance of the key junctions based on the Derived 2020 peak hour flows are calculated and presented in Table 3-3 with detailed calculation sheets presented in Appendix A.

Table 3-3 Peak Hour Junction Performances based on Derived 2020 Traffic Flows

| Jn. <br> ID. | Location | Type | Capacity <br> Index (i) | AM Peak | PM Peak |
| :---: | :--- | :---: | :---: | :---: | :---: |
| J1 | Tsing Yi Road / Sai Shan Road | Priority | DFC | 0.57 | 0.49 |
| J2 | Tsing Yi Road / Ching Hong Road | Roundabout | DFC | 0.47 | 0.43 |
| J3 | Tsing Yi Road / Kwai Tsing Road <br> Tsing Yi Bridge | Roundabout | DFC | 0.56 | 0.50 |
| J4 | Tsing Yi Interchange | Roundabout | DFC | 0.67 | 0.61 |
| J5 | Tsing Sha Highway / Tsing Yi Road / <br> Tsing Yi Hong Wan Road | Roundabout | DFC | 0.45 | 0.45 |

Notes: (1) The Capacity Index for Priority Junction and roundabout is Design Flow to Capacity Ratio (DFC)

- A DFC value less than 0.85 indicates that the junction is operating within acceptable level and a DFC greater than 1.0 indicates that the junction is overloaded.


## 4 FUTURE TRAFFIC SITUATION

### 4.1 Design Year

4.1.1 The planned operation year of the Proposed AMEC is 2025, hence, the "Design Year" for this TIA study is set as 2028, i.e. 3 years after the operation year.

### 4.2 Methodology

4.2.1 In forecasting the future traffic flows on the road network in the Study Area, references are made to the following sources of information which include:

- The forecast population and employment from the 2016-based Territorial Population and Employment Data Matrices (TPEDM) planning data published by Planning Department; and
- Planned and committed developments in the Study Area.
4.2.2 The following steps are undertaken to derive the 2028 Peak Hour Reference Flows (i.e. without the Proposed AMEC) and Design Flows (i.e. with the Proposed AMEC):

2028 Background Flows = 2020 Traffic Flows x annual growth factors

2028 Reference Flows = 2028 Background Flows + additional traffic generated by planned/committed developments

2028 Design Flows $=\quad 2028$ Reference Flows
4.2.3 As mentioned in Section 2.2 and Table 2-1, it is noted that the Proposed AMEC will not increase the total number of students / staff in the VTC TY Campus and hence would not induce additional traffic and pedestrian flows upon operation of the Proposed AMEC development. As a result, the 2028 Design Flows (i.e. with the AMEC) would be the same as the 2028 Reference Flows (without the AMEC development) as the latter scenario has already included the traffic flows generated by the existing VTC TY Campus.
4.2.4 The traffic impact of the VTC TY Campus with the Proposed AMEC is then assessed based on the 2028 Peak Hour Design Traffic Flows.

### 4.3 2028 Background Traffic Flows

4.3.1 To estimate the 2028 Background Traffic Flows, reference is made to the 2016-based Territorial Population and Employment Data Matrices (TPEDM) planning data published by Planning Department. Table 4-1 presents the population and employment data in Kwai Tsing District for 2016, 2021 and 2026.

Table 4-1 2016-Based TPEDM in Kwai Tsing District

| Category | 2016 | 2021 | 2026 | Annual Growth Rate |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | $2016-2021$ | $2021-2026$ |
| Population | 184,150 | 181,350 | 186,700 | $-0.31 \%$ | $0.58 \%$ |
| Employment Places | 37,500 | 39,150 | 39,250 | $0.86 \%$ | $0.05 \%$ |

Source: 2016, 2021 \& 2026 population and employment places are extracted from 2016-based TPEDM published by Planning Department (Dec 2019).
4.3.2 As shown in the table, the predicted population and employment growth in Kwai Tsing District is approximately $+0.58 \%$ and $+0.05 \%$ per annum respectively from 2021 to 2026. To provide conservative estimates, it is proposed to adopt the higher annual growth rate of $+0.58 \%$ for estimating the 2028 Background Traffic Flows. By applying the proposed growth rate ( $+0.58 \%$ p.a.) to the 2020 peak hour flows, the forecast 2028 Background Traffic Flows are calculated and presented in Figure 4-1.

### 4.4 2028 Reference / Design Traffic Flows

4.4.1 According to the published information from Town Planning Board, there are three planned/committed developments in the vicinity of the Project Site and these are:

- Hong Kong Housing Authority - Public Housing Development at Ching Hong Road North, Tsing Yi [Planned Completion Year: 20232028 by phases]
- Hong Kong Housing Authority - Public Housing Development at Tsing Hung Road, Tsing Yi [Planned Completion Year: 2022/23]
- Proposed Residential Development at Tsing Yi Town Lot No. 190 [Planned Completion Year: 2022].
4.4.2 The locations of the above developments are shown in Figure 4-2.
4.4.3 The additional peak hour traffic to be generated by the new developments are estimated based on the respective trip rates in TPDM as indicated in Table 4-2 and the resulting peak hour trip generations are shown in Table 4-3.

Table 4-2 Peak Hour Trip Rates for Planned/ Committed Developments

| Development Density / <br> OZP Zoning | unit | AM Peak Hour |  | PM Peak Hour |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | In | Out | In |  |
| Subsidised Housing: <br> Public Rental <br> Average Flat Size 40m | pcu/hr/flat | 0.0432 | 0.0326 | 0.0237 | 0.0301 |
| Retail / Shopping Complex <br> (Office + Retail) | pcu/hr/100m² | 0.2296 | 0.2434 | 0.3100 | 0.3563 |
| Private Housing: <br> High-Density / R(A) <br> Average Flat Size 60m² | pcu/hr/flat | 0.0718 | 0.0425 | 0.0286 | 0.0370 |

Source: TPDM Vol. 1 Chapter 3, Annex D, Table 1 and Table 2

Table 4-3 Estimated Peak Hour Trip Generations by Planned/ Committed Developments

| Location | Land Use | AM Peak Hour |  | PM Peak Hour |  |
| :--- | :---: | :---: | :---: | :---: | :---: |
|  |  | In | Out | In |  |
| Public Housing Development <br> at Ching Hong Road North, <br> Tsing Yi(1) | Public Rental Housing <br> $(3,200$ flats) | 138 | 104 | 76 | 96 |
|  | Retail <br> $\left(2,000 \mathrm{~m}^{2}\right.$ GFA) | 5 | 5 | 6 | 7 |
| Public Housing Development <br> at Tsing Hung Road, <br> Tsing Yi(1) | Public Rental Housing <br> $(2,868$ flats) | 124 | 93 | 68 | 86 |
| Retail <br> $\left(1,600 \mathrm{~m}^{2}\right.$ GFA) | 4 | 4 | 5 | 6 |  |
| Proposed Residential <br> Development at Tsing Yi <br> Town Lot No. 190(2) | Private Housing <br> $(766$ flats) | 56 | 33 | 22 | 29 |
| Total | 327 | 239 | 177 | 224 |  |

Source: (1) Development parameters from Housing Department Planning Brief published by Planning Department (Jan 2020)
(2) Development parameter published by Lands Department (Apr 2019)
4.4.4 The additional development flows in Table 4-4 are then added to the 2028 Peak Hour Background Traffic (Figure 4-1) to derive the 2028 Peak Hour Reference Traffic Flows.
4.4.5 As mentioned in Paragraph 4.2.2 and 4.2.3, the 2028 Design Flows would be the same as the Reference Flows since no additional traffic would be generated by the Proposed AMEC. The resulting 2028 Design Flows are shown in Figure 4-3.

### 4.5 2028 Junction Capacity Assessments

4.5.1 Based on the 2028 Design Flows, junction capacity assessments are undertaken and the results are presented in Table 4-4 with detailed calculation sheets provided in Appendix B.

Table 4-4 2028 Peak Hour Performance at Key Junctions

| Jn. <br> ID. | Location | Type | Capacity <br> Index(1) | AM Peak | PM Peak |
| :---: | :--- | :---: | :---: | :---: | :---: |
| J1 | Tsing Yi Road / Sai Shan Road | Priority | DFC | 0.67 | 0.56 |
| J2 | Tsing Yi Road / Ching Hong <br> Road | Roundabout | DFC | 0.54 | 0.49 |
| J3 | Tsing Yi Road / Kwai Tsing <br> Road Tsing Yi Bridge | Roundabout | DFC | 0.69 | 0.56 |
| J4 | Tsing Yi Interchange | Roundabout | DFC | 0.76 | 0.67 |
| J5 | Tsing Sha Highway / Tsing Yi <br> Road / Tsing Yi Hong Wan Road | Roundabout | DFC | 0.49 | 0.49 |

Notes: (1) The Capacity Index for Priority Junction and roundabout is Design Flow to Capacity Ratio (DFC)

- A DFC value less than 0.85 indicates that the junction is operating within acceptable level and a DFC greater than 1.0 indicates that the junction is overloaded.
4.5.2 The results show that the key junctions in the Study Area would operate within capacity during both the AM and PM peak hours in 2028 for the Design scenario (i.e. with Proposed AMEC). The proposed AMEC development would not create adverse traffic impact because the proposed development would not induce additional traffic.


## 5 PEDESTRIAN IMPACT ASSESSMENT AND PUBLIC TRANSPORT REVIEW

### 5.1 Pedestrian Impact Assessment

5.1.1 Similar to vehicular traffic, as the overall nos. of students/ staff will not be increased, the peak hour pedestrian trips observed at the existing VTC TY campus in 2017 are adopted for assessing the level of services (LOS) of various pedestrian facilities within the campus with the Proposed AMEC. Table 5-1 shows the observed peak-15 minutes pedestrian flows at the main pedestrian links near the Proposed AMEC and the locations of the concerned pedestrian links are shown in Figure 2-2.

Table 5-1 Observed Peak-15 Minute Pedestrian Trips at VTC TY Campus

| ID | Location | AM Peak 15-min Flows |  |  | PM Peak 15-min Flows |  |  |
| :---: | :--- | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Out | In | Total | Out | In | Total |
| P1 | Covered Staircase | 1 | 206 | 207 | 512 | 34 | 546 |
| P2 | Main Access to VTC Campus | 0 | 104 | 104 | 83 | 33 | 116 |
| P3 | Access to Indoor Carpark | 1 | 25 | 26 | 23 | 5 | 28 |
| P4 | Access to Internal Access Road | 6 | 8 | 14 | 22 | 4 | 26 |
|  | Total | $\mathbf{8}$ | 343 | 351 | 640 | 76 | 716 |

Source: Technical Study for Aircraft and Marine Engineering Centre at Tsing Yi Campus Traffic Impact Study (November 2017), Table 6.1
Notes: (1) refer to Figure 2-2 for locations of pedestrian links.
5.1.2 The performances of footpaths P2, P3 and P4 are assessed based on the Level of Service (LOS) method in accordance with the Transport Planning and Design Manual (Chapter 10.4.2, Volume 6). The definitions of different level of LOS on footpaths are described in Table 5-2 and shown graphically in Exihit-1.

Table 5-2 Description of Level-of-Service (LOS) on Footpaths

| LOS | Flow Rate (ped/min/m) | Description |
| :---: | :---: | :---: |
| A | $\leq 16$ | Pedestrians basically move in desired paths without altering their movements in response to other pedestrians. Walking speeds are freely selected, and conflicts between pedestrians are unlikely. |
| B | 16-23 | Sufficient space is provided for pedestrians to freely select their walking speeds, to bypass other pedestrians and to avoid crossing conflicts with others. At this level, pedestrians begin to be aware of other pedestrians and to respond to their presence in the selection of walking paths. |
| C | 23-33 | Sufficient space is available to select normal walking speeds and to bypass other pedestrians primarily in unidirectional stream. Where reverse direction or crossing movement exists, minor conflicts will occur, and speed and volume will be somewhat lower. |
| D | 33-49 | Freedom to select individual walking speeds and bypass other pedestrians is restricted. Where crossing or reverse-flow movements exist, the probability of conflicts is high and its avoidance requires changes of speeds and position. The LOS provides reasonable fluid flow; however considerable friction and interactions between pedestrians are likely to occur. |
| E | 49-75 | Virtually, all pedestrians would have their normal walking speeds restricted. At the lower range of this LOS, forward movement is possible only by shuffling. Space is insufficient to pass over slower pedestrians. Cross- and reverse-movement are possible only with extreme difficulties. Design volumes approach the limit of walking capacity with resulting stoppages and interruptions to flow. |
| F | > 75 | Walking speeds are severely restricted. Forward progress is made only by shuffling. There are frequent and unavoidable conflicts with other pedestrians. Cross- and reverse-movements are virtually impossible. Flow is sporadic and unstable. Space is more characteristics of queued pedestrians than of moving pedestrian streams. |

Exhibit-1 Graphical Presentation of Level of Service (LOS)

5.1.3 The performance of stairs P 1 is assessed with reference to the guidelines in Highway Capacity Manual 2010 and as described in Table 5-3.

Table 5-3 Description of Level-of-Service (LOS) for Stairs

| LOS | Flow Rate <br> (ped/min/m) | Description |
| :---: | :---: | :--- |
| A | $\leq 16$ | Sufficient area is provided to freely select locomotion speed, <br> and to bypass other slower-moving pedestrians. No serious <br> difficulties would be experienced with reverse traffic flows. |
| B | $16-20$ | Lower range of area occupancy, some difficulties would be <br> experienced in passing slower pedestrians. Reverse flows <br> would cause minor traffic conflicts. |
| C | $20-26$ | Locomotion speeds would be restricted slightly, due to an <br> inability to pass slower-moving pedestrians. Minor reverse <br> traffic flows would encounter some difficulties. |
| D | $26-36$ | Locomotion speeds are restricted for the majority of persons, <br> due to the limited open tread space and an inability to bypass <br> slower-moving pedestrians. Reverse flows would encounter <br> significant difficulties and traffic conflict. |
| E | $36-49$ | Virtually all persons would have their normal locomotion speeds <br> reduced, because of the minimum tread length, space and <br> inability to bypass others, intermittent stoppages are likely to to <br> occur. Reverse traffic flows would experience serious conflict. |
| F | $>49$ | Completed breakdown in traffic flow, with many stoppages. |

5.1.4 The LOS of P1, P2, P3 and P4 for the future VTC Campus with the Proposed AMEC are assessed and the results are indicated in Table 5-4.

Table 5-4 Level of Services (LOS) Assessment Results

| Location ${ }^{(2)}$ | Effective Width ${ }^{(1)}$ | AM Peak Hour |  |  | PM Peak hour |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Peak 15-min 2-way Flow | Flow Rate (ped/min/m) | LOS | Peak 15-min 2-way Flow | Flow Rate (ped/min/m) | LOS |
| P1 | 4.3 | 207 | 3.2 | A | 546 | 8.5 | A |
| P2 | 3.3 | 104 | 2.1 | A | 116 | 2.3 | A |
| P3 | 3.0 | 26 | 0.6 | A | 28 | 0.6 | A |
| P4 | 0.6 | 14 | 1.6 | A | 26 | 2.9 | A |
| Notes: (1) Effective width = Actual width minus 1.0 m shy zone <br> (2) Refer to Figure 2-2 for location of pedestrian link |  |  |  |  |  |  |  |

5.1.5 The results indicate that LOS A could be achieved at all the concerned footpaths for both the AM and PM peak hours, i.e. indicating that the pedestrian links have sufficient capacity to accommodate the pedestrian flows with the Proposed AMEC.

### 5.2 Public Transport Review

5.2.1 At present, around $65 \%$ of the students adopt public transport services, including franchised bus and minibus services, to access the VTC TY Campus. Since the Proposed AMEC will not generate additional students, the demand for public transport services after the operation of the Proposed AMEC would be similar to the existing situation, i.e. no additional public transport services would be required.

## 6 SUMMARY AND CONCLUSIONS

### 6.1 Summary

6.1.1 The Vocational Training Council (VTC) intend to redevelop the northern portion of the existing VTC campus in Tsing Yi for an Aviation and Maritime Education Centre (AMEC) which will provide workshops, laboratories, teaching facilities, staff offices and associated facilities to provide practical training for 1000 nos. of students who come from the related programmes offered at the TY Campus in each academic year, i.e. the Proposed AMEC will not generate additional students/ staff.
6.1.2 Ozzo Technology (HK) Limited are commissioned to undertake this Traffic Impact Assessment (TIA) Study to assess the traffic impact on the nearby road network after the completion of the Proposed AMEC in 2025.
6.1.3 The Project Site is well served by public transport, including franchised bus, GMB services and VTC shuttle bus services. Due to the abnormal traffic conditions in the territory as a result of the outbreak of coronavirus diseases, reference is made to traffic and pedestrian data obtained in 2017, in which school activities are normal, as the basis for estimating the future traffic.
6.1.4 The planned completion for the Proposed Development is 2025 and hence the "Design Year" for this study is set as 2028, i.e. 3 years after the completion year. The 2028 Background Traffic Flows are estimated taking into account the historical trend of traffic growth in the area and the forecast development intensity in the area.
6.1.5 The peak hour trips to be generated by the planned and committed developments are added to the 2028 Peak Hour Background Flows to derive the 2028 Peak Hour Reference Flows (i.e. without the Proposed Development). Since the Proposed AMEC will not increase the no. of students/staff in the VTC TY Campus, no additional traffic would therefore be generated by the Proposed AMEC, the 2028 Peak Hour Design Flows (i.e. with the Proposed Development) will be the same as the 2028 Reference Flows.
6.1.6 Junction Capacity assessments are undertaken based on the 2028 Peak Hour Design Flows (i.e. with the Proposed AMEC). The assessment results indicate that all the key junctions in the vicinity of the proposed development would perform satisfactorily during the AM and PM peak periods.

Traffic ImpactAssessment Study
6.1.7 Pedestrian impact assessments are also undertaken to assess the performance of the stairs and footpaths at the accesses to VTC campus. The results of the assessments indicate that the concerned stairs and footpaths would perform satisfactorily with sufficient spare capacity during the peak hour with the operation of the Proposed AMEC.
6.1.8 Since the Proposed AMEC will not generate additional students, the demand for public transport services after the operation of the Proposed AMEC would be similar to the existing situation, i.e. no additional public transport services would be required.

### 6.2 Conclusions

6.2.1 In view of the traffic impact assessment results, it is concluded that the Proposed AMEC Development would not create adverse impact on the surrounding road network and public transport services.

## Figures











## Appendix A

## 2020 Junction Calculation Sheets





| ARM |  |  | A | B | c | D |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| INPUT PARAMETERS: |  |  |  |  |  |  |  |  |  |
|  | $=$ | Approach half width (m) | 7.0 | 7.2 | 5.0 | 0.0 |  |  |  |
|  | $=$ | Entry width (m) | 7.6 | 8.7 | 9.2 | 0.0 |  |  |  |
| L | $=$ | Effective length of flare (m) | 3.4 | 5.8 | 14.7 | 0.0 |  |  |  |
| R | $=$ | Entry radius (m) | 23.1 | 24.3 | 24.1 | 0.0 |  |  |  |
| D | $=$ | Inscribed circle diameter (m) | 30.0 | 30.0 | 30.0 | 0.0 |  |  |  |
| A | $=$ | Entry angle (degree) | 10.0 | 28.0 | 20.0 | 0.0 |  |  |  |
| Q | $=$ | Entry flow (pcu/h) | 780 | 1098 | 329 | 0 |  |  |  |
| Qc | $=$ | Circulating flow across entry (pcu/h) | 479 | 135 | 764 | 0 |  |  |  |
| OUTPUT PARAMETERS: |  |  |  |  |  |  |  |  |  |
| S | = | Sharpness of flare $=1.6(\mathrm{E}-\mathrm{V}) / \mathrm{L}$ | 0.29 | 0.42 | 0.45 | 0.00 |  |  |  |
|  | $=$ | 1-0.00347(A-30)-0.978(1/R-0.05) | 1.08 | 1.02 | 1.04 | 0.00 |  |  |  |
|  | $=$ | $\mathrm{V}+((\mathrm{E}-\mathrm{V}) /(1+2 \mathrm{~S})$ ) | 7.39 | 8.02 | 7.22 | 0.00 |  |  |  |
| M | $=$ | $\operatorname{EXP}((\mathrm{D}-60) / 10)$ | 0 | 0 | 0 | 0 |  |  |  |
| F | $=$ | 303*X2 | 2240 | 2429 | 2188 | 0 |  |  |  |
| Td | = | 1+(0.5/(1+M)) | 1.48 | 1.48 | 1.48 | 0.00 |  |  |  |
| Fc | $=$ | $0.21 * \operatorname{Td}\left(1+0.2^{*} \mathrm{X} 2\right)$ | 0.77 | 0.81 | 0.76 | 0.00 |  |  |  |
| Qe | $=$ | $\mathrm{K}(\mathrm{F}-\mathrm{Fc} * \mathrm{Qc})$ | 2014 | 2357 | 1678 | 0 | Total In Sum = | 2207 | PCU |
| DFC | = | Design flow/Capacity = Q/Qe | 0.39 | 0.47 | 0.20 | 0.00 | DFC of Critical Approach = | 0.47 |  |



| ARM |  |  | A | B | c | D |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| INPUT PARAMETERS: |  |  |  |  |  |  |  |  |  |
| V | $=$ | Approach half width (m) | 7.0 | 7.2 | 5.0 | 0.0 |  |  |  |
| E | $=$ | Entry width (m) | 7.6 | 8.7 | 9.2 | 0.0 |  |  |  |
| L | = | Effective length of flare (m) | 3.4 | 5.8 | 14.7 | 0.0 |  |  |  |
| R | = | Entry radius (m) | 23.1 | 24.3 | 24.1 | 0.0 |  |  |  |
| D | $=$ | Inscribed circle diameter (m) | 30.0 | 30.0 | 30.0 | 0.0 |  |  |  |
| A | = | Entry angle (degree) | 10.0 | 28.0 | 20.0 | 0.0 |  |  |  |
| Q | = | Entry flow (pcu/h) | 678 | 1001 | 318 | 0 |  |  |  |
| Qc | $=$ | Circulating flow across entry (pcu/h) | 404 | 156 | 737 | 0 |  |  |  |
| OUTPUT PARAMETERS: |  |  |  |  |  |  |  |  |  |
| S | = | Sharpness of flare $=1.6(\mathrm{E}-\mathrm{V}) / \mathrm{L}$ | 0.29 | 0.42 | 0.45 | 0.00 |  |  |  |
| K | $=$ | 1-0.00347(A-30)-0.978(1/R-0.05) | 1.08 | 1.02 | 1.04 | 0.00 |  |  |  |
| X2 | = | $\mathrm{V}+((\mathrm{E}-\mathrm{V}) /(1+2 \mathrm{~S})$ ) | 7.39 | 8.02 | 7.22 | 0.00 |  |  |  |
| M | = | $\operatorname{EXP}((\mathrm{D}-60) / 10)$ | 0 | 0 | 0 | 0 |  |  |  |
| F | = | 303*X2 | 2240 | 2429 | 2188 | 0 |  |  |  |
| Td | = | 1+(0.5/(1+M)) | 1.48 | 1.48 | 1.48 | 0.00 |  |  |  |
| Fc | $=$ | $0.21 * T d\left(1+0.2^{*} \mathrm{X} 2\right)$ | 0.77 | 0.81 | 0.76 | 0.00 |  |  |  |
| Qe | = | $\mathrm{K}\left(\mathrm{F}-\mathrm{Fc}^{*} \mathrm{Qc}\right)$ | 2076 | 2340 | 1699 | 0 | Total In Sum = | 1997 | PCU |
| DFC | $=$ | Design flow/Capacity = Q/Qe | 0.33 | 0.43 | 0.19 | 0.00 | DFC of Critical Approach = | 0.43 |  |





| ARM |  | A | B |
| :---: | :---: | :---: | :---: |
| INPUT PARAMETERS: |  |  |  |
|  | $=$ Approach half width ( m ) | 5.8 | 7.4 |
|  | $=\quad$ Entry width (m) | 9.2 | 8.7 |
| L | $=$ Effective length of flare (m) | 4.8 | 7.1 |
| R | $=$ Entry radius (m) | 18.1 | 44.5 |
| D | $=$ Inscribed circle diameter ( m ) | 60.0 | 60.0 |
| A | = Entry angle (degree) | 45.0 | 29.0 |
| Q | = Entry flow (pcu/h) | 323 | 1711 |
|  | $=$ Circulating flow across entry (pcu/h) | 1173 | 6 |
| OUTPUT PARAMETERS: |  |  |  |
|  | $=\quad$ Sharpness of flare $=1.6(\mathrm{E}-\mathrm{V}) / \mathrm{L}$ | 1.14 | 0.30 |
| K | $=1-0.00347(\mathrm{~A}-30)-0.978(1 / \mathrm{R}-0.05)$ | 0.94 | 1.03 |
|  | $=\quad \mathrm{V}+((\mathrm{E}-\mathrm{V}) /(1+2 S))$ | 6.87 | 8.23 |
| M | $=\operatorname{EXP}((\mathrm{D}-60) / 10)$ | 1 | 1 |
| F | 303*X2 | 2081 | 2494 |
|  | $=1+(0.5 /(1+\mathrm{M})$ ) | 1.25 | 1.25 |
| Fc | $=0.21^{*} \mathrm{Td}\left(1+0.2^{*} \times 2\right)$ | 0.62 | 0.69 |
|  | $=\mathrm{K}\left(\mathrm{F}-\mathrm{Fc}{ }^{*}\right.$ Qc $)$ | 1273 | 2565 |
| DFC | $=$ Design flow/Capacity $=\mathrm{Q} / \mathrm{Qe}$ | 0.25 | 0.67 |



| ARM |  | A | B |
| :---: | :---: | :---: | :---: |
| INPUT PARAMETERS: |  |  |  |
| v | $=\quad$ Approach half width (m) | 5.8 | 7.4 |
| E | $=\quad$ Entry width (m) | 9.2 | 8.7 |
|  | $=$ Effective length of flare ( m ) | 4.8 | 7.1 |
| R | $=$ Entry radius (m) | 18.1 | 44.5 |
| D | $=\quad$ Inscribed circle diameter (m) | 60.0 | 60.0 |
| A | = Entry angle (degree) | 45.0 | 29.0 |
| Q | $=$ Entry flow (pcu/h) | 264 | 1560 |
|  | = Circulating flow across entry (pcu/h) | 856 | 6 |
| OUTPUT PARAMETERS: |  |  |  |
| s | $=\quad$ Sharpness of flare $=1.6(\mathrm{E}-\mathrm{V}) / \mathrm{L}$ | 1.14 | 0.30 |
| K | $=1-0.00347(\mathrm{~A}-30)-0.978(1 / \mathrm{R}-0.05)$ | 0.94 | 1.03 |
| X2 | $=\quad \mathrm{V}+((\mathrm{E}-\mathrm{V}) /(1+2 \mathrm{~S})$ ) | 6.87 | 8.23 |
| M | $=\operatorname{EXP}((\mathrm{D}-60) / 10)$ | 1 | 1 |
| F | $=303 * \times 2$ | 2081 | 2494 |
| Td | $=1+(0.5 /(1+\mathrm{M})$ ) | 1.25 | 1.25 |
| Fc | $=0.21 * T \mathrm{~T}(1+0.2 * \times 2)$ | 0.62 | 0.69 |
|  | $=\mathrm{K}\left(\mathrm{F}-\mathrm{Fc}{ }^{*}\right.$ Qc) | 1460 | 2565 |
| DFC | $=$ Design flow/Capacity $=\mathrm{Q} / \mathrm{Qe}$ | 0.18 | 0.61 |



| ARM |  | A | B | C | D |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| INPUT PARAMETERS: |  |  |  |  |  |  |  |  |
| v | = Approach half width ( m ) | 11.1 | 9.1 | 8.0 | 11.4 |  |  |  |
| E | $=$ Entry width (m) | 15.1 | 13.9 | 13.2 | 12.4 |  |  |  |
| L | $=$ Effective length of flare ( $m$ ) | 27.6 | 9.9 | 9.3 | 9.8 |  |  |  |
| R | $=$ Entry radius (m) | 45.9 | 29.5 | 77.1 | 73.4 |  |  |  |
| D | $=$ Inscribed circle diameter ( m ) | 100.0 | 100.0 | 100.0 | 100.0 |  |  |  |
| A | = Entry angle (degree) | 18.0 | 14.0 | 16.0 | 12.0 |  |  |  |
| Q | = Entry flow (pcu/h) | 1205 | 1259 | 1017 | 807 |  |  |  |
| Qc | $=$ Circulating flow across entry (pcu/h) | 619 | 947 | 1453 | 1657 |  |  |  |
| OUTPUT PARAMETERS: |  |  |  |  |  |  |  |  |
| s | $=$ Sharpness of flare $=1.6(\mathrm{E}-\mathrm{V}) / \mathrm{L}$ | 0.23 | 0.78 | 0.91 | 0.16 |  |  |  |
| K | $=1-0.00347(\mathrm{~A}-30)-0.978(1 / \mathrm{R}-0.05)$ | 1.07 | 1.07 | 1.08 | 1.10 |  |  |  |
| X2 | $=\quad \mathrm{V}+((\mathrm{E}-\mathrm{V}) /(1+2 \mathrm{~S})$ ) | 13.82 | 10.94 | 9.82 | 12.18 |  |  |  |
| M | $=\operatorname{EXP}((\mathrm{D}-60) / 10)$ | 55 | 55 | 55 | 55 |  |  |  |
| F | $=303^{*} \times 2$ | 4188 | 3314 | 2976 | 3692 |  |  |  |
| Td | $=1+(0.5 /(1+\mathrm{M})$ ) | 1.01 | 1.01 | 1.01 | 1.01 |  |  |  |
| Fc | $=0.21^{*} \mathrm{Td}\left(1+0.2^{*} \times 2\right)$ | 0.80 | 0.68 | 0.63 | 0.73 |  |  |  |
| Qe | $=\mathrm{K}\left(\mathrm{F}-\mathrm{Fc}{ }^{*}\right.$ Qc) | 3950 | 2865 | 2239 | 2729 | Total In Sum = | 4288 | PCU |
| DFC | = Design flow/Capacity $=\mathrm{Q} / \mathrm{Qe}$ | 0.31 | 0.44 | 0.45 | 0.30 | DFC of Critical Approach $=$ | 0.45 |  |



| ARM |  | A | B | C | D |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| INPUT PARAMETERS: |  |  |  |  |  |  |  |  |
| v | = Approach half width ( m ) | 11.1 | 9.1 | 8.0 | 11.4 |  |  |  |
| E | $=$ Entry width (m) | 15.1 | 13.9 | 13.2 | 12.4 |  |  |  |
| L | $=$ Effective length of flare ( $m$ ) | 27.6 | 9.9 | 9.3 | 9.8 |  |  |  |
| R | $=$ Entry radius (m) | 45.9 | 29.5 | 77.1 | 73.4 |  |  |  |
| D | $=$ Inscribed circle diameter ( m ) | 100.0 | 100.0 | 100.0 | 100.0 |  |  |  |
| A | = Entry angle (degree) | 18.0 | 14.0 | 16.0 | 12.0 |  |  |  |
| Q | = Entry flow (pcu/h) | 753 | 947 | 1017 | 770 |  |  |  |
| Qc | $=$ Circulating flow across entry (pcu/h) | 377 | 1393 | 1442 | 1576 |  |  |  |
| OUTPUT PARAMETERS: |  |  |  |  |  |  |  |  |
| s | $=$ Sharpness of flare $=1.6(\mathrm{E}-\mathrm{V}) / \mathrm{L}$ | 0.23 | 0.78 | 0.91 | 0.16 |  |  |  |
| K | $=1-0.00347(\mathrm{~A}-30)-0.978(1 / \mathrm{R}-0.05)$ | 1.07 | 1.07 | 1.08 | 1.10 |  |  |  |
| X2 | $=\quad \mathrm{V}+((\mathrm{E}-\mathrm{V}) /(1+2 \mathrm{~S})$ ) | 13.82 | 10.94 | 9.82 | 12.18 |  |  |  |
| M | $=\operatorname{EXP}((\mathrm{D}-60) / 10)$ | 55 | 55 | 55 | 55 |  |  |  |
| F | $=303^{*} \times 2$ | 4188 | 3314 | 2976 | 3692 |  |  |  |
| Td | $=1+(0.5 /(1+\mathrm{M})$ ) | 1.01 | 1.01 | 1.01 | 1.01 |  |  |  |
| Fc | $=0.21^{*} \mathrm{Td}\left(1+0.2^{*} \times 2\right)$ | 0.80 | 0.68 | 0.63 | 0.73 |  |  |  |
| Qe | $=\mathrm{K}\left(\mathrm{F}-\mathrm{Fc}{ }^{*}\right.$ Qc) | 4156 | 2542 | 2246 | 2793 | Total In Sum = | 3487 | PCU |
| DFC | = Design flow/Capacity $=\mathrm{Q} / \mathrm{Qe}$ | 0.18 | 0.37 | 0.45 | 0.28 | DFC of Critical Approach $=$ | 0.45 |  |

## Appendix B

## 2028 Junction Calculation Sheets





| ARM |  | A | B | c | D |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| INPUT PARAMETERS: |  |  |  |  |  |  |  |  |
|  | = Approach half width (m) | 7.0 | 7.2 | 5.0 | 0.0 |  |  |  |
| E | $=$ Entry width (m) | 7.6 | 8.7 | 9.2 | 0.0 |  |  |  |
| L | $=$ Effective length of flare (m) | 3.4 | 5.8 | 14.7 | 0.0 |  |  |  |
| R | $=$ Entry radius (m) | 23.1 | 24.3 | 24.1 | 0.0 |  |  |  |
| D | $=\quad$ Inscribed circle diameter (m) | 30.0 | 30.0 | 30.0 | 0.0 |  |  |  |
| A | = Entry angle (degree) | 10.0 | 28.0 | 20.0 | 0.0 |  |  |  |
| Q | = Entry flow (pcu/h) | 847 | 1258 | 525 | 0 |  |  |  |
| Qc | $=$ Circulating flow across entry (pcu/h) | 646 | 166 | 807 | 0 |  |  |  |
| OUTPUT PARAMETERS: |  |  |  |  |  |  |  |  |
| S | $=$ Sharpness of flare $=1.6(\mathrm{E}-\mathrm{V}) / \mathrm{L}$ | 0.29 | 0.42 | 0.45 | 0.00 |  |  |  |
| K | $=1-0.00347(\mathrm{~A}-30)-0.978(1 / \mathrm{R}-0.05)$ | 1.08 | 1.02 | 1.04 | 0.00 |  |  |  |
| X2 | $=\quad \mathrm{V}+((\mathrm{E}-\mathrm{V}) /(1+2 \mathrm{~S})$ ) | 7.39 | 8.02 | 7.22 | 0.00 |  |  |  |
|  | $=\operatorname{EXP}((\mathrm{D}-60) / 10)$ | 0 | 0 | 0 | 0 |  |  |  |
| F | $=303 * \times 2$ | 2240 | 2429 | 2188 | 0 |  |  |  |
|  | $=1+(0.5 /(1+\mathrm{M})$ ) | 1.48 | 1.48 | 1.48 | 0.00 |  |  |  |
| Fc | $=0.21^{*} \mathrm{Td}\left(1+0.2^{*} \mathrm{X} 2\right)$ | 0.77 | 0.81 | 0.76 | 0.00 |  |  |  |
|  | $=\mathrm{K}\left(\mathrm{F}-\mathrm{Fc}{ }^{*} \mathrm{Qc}\right)$ | 1876 | 2331 | 1644 | 0 | Total In Sum = | 2630 | PCU |
| DFC | $=$ Design flow/Capacity $=\mathrm{Q} / \mathrm{Qe}$ | 0.45 | 0.54 | 0.32 | 0.00 | DFC of Critical Approach $=$ | 0.54 |  |



| ARM |  |  | A | B | C | D |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| INPUT PARAMETERS: |  |  |  |  |  |  |  |  |  |
|  | $=$ | Approach half width (m) | 7.0 | 7.2 | 5.0 | 0.0 |  |  |  |
|  | $=$ | Entry width (m) | 7.6 | 8.7 | 9.2 | 0.0 |  |  |  |
| L | $=$ | Effective length of flare (m) | 3.4 | 5.8 | 14.7 | 0.0 |  |  |  |
| R | $=$ | Entry radius (m) | 23.1 | 24.3 | 24.1 | 0.0 |  |  |  |
|  | $=$ | Inscribed circle diameter (m) | 30.0 | 30.0 | 30.0 | 0.0 |  |  |  |
| A | $=$ | Entry angle (degree) | 10.0 | 28.0 | 20.0 | 0.0 |  |  |  |
| Q | $=$ | Entry flow (pcu/h) | 738 | 1144 | 423 | 0 |  |  |  |
| Qc | $=$ | Circulating flow across entry (pcu/h) | 495 | 186 | 776 | 0 |  |  |  |
| OUTPUT PARAMETERS: |  |  |  |  |  |  |  |  |  |
| s | $=$ | Sharpness of flare $=1.6(\mathrm{E}-\mathrm{V}) / \mathrm{L}$ | 0.29 | 0.42 | 0.45 | 0.00 |  |  |  |
| K | $=$ | 1-0.00347(A-30)-0.978(1/R-0.05) | 1.08 | 1.02 | 1.04 | 0.00 |  |  |  |
| X2 | $=$ | $\mathrm{V}+((\mathrm{E}-\mathrm{V}) /(1+2 \mathrm{~S})$ ) | 7.39 | 8.02 | 7.22 | 0.00 |  |  |  |
|  | $=$ | $\operatorname{EXP}((\mathrm{D}-60) / 10)$ | 0 | 0 | 0 | 0 |  |  |  |
| F | $=$ | 303*X2 | 2240 | 2429 | 2188 | 0 |  |  |  |
| Td | $=$ | 1+(0.5/(1+M)) | 1.48 | 1.48 | 1.48 | 0.00 |  |  |  |
| Fc | $=$ | $0.21 * \mathrm{Td}\left(1+0.2^{*} \mathrm{X} 2\right)$ | 0.77 | 0.81 | 0.76 | 0.00 |  |  |  |
| Qe | $=$ | $\mathrm{K}\left(\mathrm{F}-\mathrm{Fc}{ }^{*} \mathrm{Qc}\right)$ | 2001 | 2315 | 1669 | 0 | Total In Sum = | 2306 | PCU |
| DFC | = | Design flow/Capacity = Q/Qe | 0.37 | 0.49 | 0.25 | 0.00 | DFC of Critical Approach = | 0.49 |  |



| ARM |  | A | B | c | D |
| :---: | :---: | :---: | :---: | :---: | :---: |
| INPUT PARAMETERS: |  |  |  |  |  |
|  | $=$ Approach half width ( m ) | 7.5 | 7.2 | 7.8 | 7.5 |
| E | = Entry width (m) | 10.3 | 10.1 | 11.4 | 9.3 |
| L | $=$ Effective length of flare (m) | 5.9 | 5.0 | 6.2 | 3.2 |
| R | $=$ Entry radius (m) | 21.5 | 43.4 | 10.2 | 33.7 |
| D | = Inscribed circle diameter (m) | 60.0 | 60.0 | 60.0 | 60.0 |
| A | = Entry angle (degree) | 34.0 | 32.0 | 60.0 | 33.0 |
| Q | $=$ Entry flow (pcu/h) | 420 | 792 | 1048 | 1351 |
| Qc | = Circulating flow across entry (pcu/h) | 147 | 562 | 977 | 753 |
| OUTPUT PARAMETERS: |  |  |  |  |  |
| s | $=$ Sharpness of flare $=1.6(\mathrm{E}-\mathrm{V}) / \mathrm{L}$ | 0.77 | 0.93 | 0.93 | 0.92 |
| K | $=1-0.00347(\mathrm{~A}-30)-0.978(1 / \mathrm{R}-0.05)$ | 0.99 | 1.02 | 0.85 | 1.01 |
| X2 | $=\quad \mathrm{V}+((\mathrm{E}-\mathrm{V})(1+2 \mathrm{~S})$ ) | 8.58 | 8.23 | 9.02 | 8.15 |
| M | $=\operatorname{EXP}((\mathrm{D}-60) / 10)$ | 1 | 1 | 1 | 1 |
| F | 303*X2 | 2600 | 2494 | 2733 | 2469 |
| Td | $=1+(0.5 /(1+\mathrm{M})$ ) | 1.25 | 1.25 | 1.25 | 1.25 |
| Fc | $=0.21^{*} \mathrm{Td}\left(1+0.2^{*} \mathrm{X} 2\right)$ | 0.71 | 0.69 | 0.74 | 0.69 |
|  | $=\mathrm{K}\left(\mathrm{F}-\mathrm{Fc}{ }^{*}\right.$ Qc) | 2469 | 2145 | 1711 | 1968 |
| DFC | $=$ Design flow/Capacity $=$ Q/Qe | 0.17 | 0.37 | 0.61 | 0.69 |




| ARM |  | A | B |
| :---: | :---: | :---: | :---: |
| INPUT PARAMETERS: |  |  |  |
| v | $=$ Approach half width ( m ) | 5.8 | 7.4 |
| E | $=$ Entry width (m) | 9.2 | 8.7 |
| L | $=$ Effective length of flare ( m ) | 4.8 | 7.1 |
| R | $=$ Entry radius (m) | 18.1 | 44.5 |
| D | $=\quad$ Inscribed circle diameter ( m ) | 60.0 | 60.0 |
| A | = Entry angle (degree) | 45.0 | 29.0 |
| Q | = Entry flow (pcu/h) | 363 | 1957 |
| Qc | $=$ Circulating flow across entry (pcu/h) | 1361 | 6 |
| OUTPUT PARAMETERS: |  |  |  |
| s | $=$ Sharpness of flare $=1.6(\mathrm{E}-\mathrm{V}) / \mathrm{L}$ | 1.14 | 0.30 |
| K | $=1-0.00347(\mathrm{~A}-30)-0.978(1 / \mathrm{R}-0.05)$ | 0.94 | 1.03 |
| X2 | $=\quad \mathrm{V}+((\mathrm{E}-\mathrm{V}) /(1+2 \mathrm{~S})$ ) | 6.87 | 8.23 |
| M | $=\operatorname{EXP}((\mathrm{D}-60) / 10)$ | 1 | 1 |
| F | $=303 * \times 2$ | 2081 | 2494 |
| Td | $=1+(0.5 /(1+\mathrm{M})$ ) | 1.25 | 1.25 |
| Fc | $=0.21 * \mathrm{Td}\left(1+0.2^{*} \mathrm{X} 2\right)$ | 0.62 | 0.69 |
|  | $=\mathrm{K}\left(\mathrm{F}-\mathrm{Fc}{ }^{*} \mathrm{Qc}\right)$ | 1163 | 2565 |
| DFC | $=$ Design flow/Capacity $=$ Q/Qe | 0.31 | 0.76 |



| ARM |  | A | B |
| :---: | :---: | :---: | :---: |
| INPUT PARAMETERS: |  |  |  |
|  | $=$ Approach half width ( m ) | 5.8 | 7.4 |
| E | = Entry width (m) | 9.2 | 8.7 |
| L | $=$ Effective length of flare ( m ) | 4.8 | 7.1 |
| R | = Entry radius (m) | 18.1 | 44.5 |
| D | = Inscribed circle diameter ( m ) | 60.0 | 60.0 |
| A | = Entry angle (degree) | 45.0 | 29.0 |
| Q | = Entry flow (pcu/h) | 300 | 1720 |
| Qc | = Circulating flow across entry (pcu/h) | 966 | 6 |
| OUTPUT PARAMETERS: |  |  |  |
|  | $=$ Sharpness of flare $=1.6(\mathrm{E}-\mathrm{V}) / \mathrm{L}$ | 1.14 | 0.30 |
| K | $=1-0.00347(\mathrm{~A}-30)-0.978(1 / \mathrm{R}-0.05)$ | 0.94 | 1.03 |
| X2 | $=\quad \mathrm{V}+((\mathrm{E}-\mathrm{V}) /(1+2 \mathrm{~S})$ ) | 6.87 | 8.23 |
| M | $=\operatorname{EXP}((\mathrm{D}-60) / 10)$ | 1 | 1 |
| F | 303*X2 | 2081 | 2494 |
|  | $=1+(0.5 /(1+\mathrm{M})$ ) | 1.25 | 1.25 |
| Fc | $=0.21^{*} \mathrm{Td}\left(1+0.2^{*} \mathrm{X} 2\right)$ | 0.62 | 0.69 |
|  | $=\mathrm{K}\left(\mathrm{F}-\mathrm{Fc}{ }^{*} \mathrm{Qc}\right)$ | 1395 | 2565 |
| DFC | $=$ Design flow/Capacity $=\mathrm{Q} / \mathrm{Qe}$ | 0.21 | 0.67 |




| ARM |  | A | B | C | D |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| INPUT PARAMETERS: |  |  |  |  |  |  |  |  |
| V | $=$ Approach half width ( m ) | 11.1 | 9.1 | 8.0 | 11.4 |  |  |  |
| E | $=$ Entry width (m) | 15.1 | 13.9 | 13.2 | 12.4 |  |  |  |
| L | $=$ Effective length of flare ( m ) | 27.6 | 9.9 | 9.3 | 9.8 |  |  |  |
| R | $=$ Entry radius (m) | 45.9 | 29.5 | 77.1 | 73.4 |  |  |  |
| D | $=$ Inscribed circle diameter ( m ) | 100.0 | 100.0 | 100.0 | 100.0 |  |  |  |
| A | = Entry angle (degree) | 18.0 | 14.0 | 16.0 | 12.0 |  |  |  |
| Q | = Entry flow (pcu/h) | 799 | 992 | 1070 | 816 |  |  |  |
| Qc | = Circulating flow across entry (pcu/h) | 397 | 1471 | 1516 | 1654 |  |  |  |
| OUTPUT PARAMETERS: |  |  |  |  |  |  |  |  |
| S | $=$ Sharpness of flare $=1.6(\mathrm{E}-\mathrm{V}) / \mathrm{L}$ | 0.23 | 0.78 | 0.91 | 0.16 |  |  |  |
| K | $=1-0.00347(\mathrm{~A}-30)-0.978(1 / \mathrm{R}-0.05)$ | 1.07 | 1.07 | 1.08 | 1.10 |  |  |  |
| X2 | $=\quad \mathrm{V}+((\mathrm{E}-\mathrm{V}) /(1+2 \mathrm{~S})$ ) | 13.82 | 10.94 | 9.82 | 12.18 |  |  |  |
| M | $=\operatorname{EXP}((\mathrm{D}-60) / 10)$ | 55 | 55 | 55 | 55 |  |  |  |
| F | $=303 * \times 2$ | 4188 | 3314 | 2976 | 3692 |  |  |  |
| Td | $=1+(0.5 /(1+\mathrm{M})$ ) | 1.01 | 1.01 | 1.01 | 1.01 |  |  |  |
| Fc | $=0.21^{*} \mathrm{Td}\left(1+0.2^{*} \mathrm{X} 2\right)$ | 0.80 | 0.68 | 0.63 | 0.73 |  |  |  |
| Qe | $=\mathrm{K}\left(\mathrm{F}-\mathrm{Fc}{ }^{*}\right.$ Qc $)$ | 4139 | 2486 | 2196 | 2731 | Total In Sum = | 3677 | PCU |
| DFC | $=$ Design flow/Capacity $=\mathrm{Q} / \mathrm{Qe}$ | 0.19 | 0.40 | 0.49 | 0.30 | DFC of Critical Approach $=$ | 0.49 |  |


[^0]:    ${ }^{1}$ 根據職訓局的初步計劃，職訓局會因應當時的實際情況，包括行業發展情況，人力需求等，考慮開辦 6個新課程。在此初步計劃下，有關航空及航海相關課程長遠規劃入學人數，亦會由 2020／21學年的 786增至 2025／26學年的約 1500 。

[^1]:    1 "Technical Study for Aircraft and Marine Engineering Centre at Tsing Yi Campus Traffic Impact Study (November 2017)"

